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McCune

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(54) **AC/DC POWER CONVERSION METHODS
AND APPARATUS**

(76) Inventor: **Earl W. McCune**, Santa Clara, CA (US)

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See application file for complete search history.

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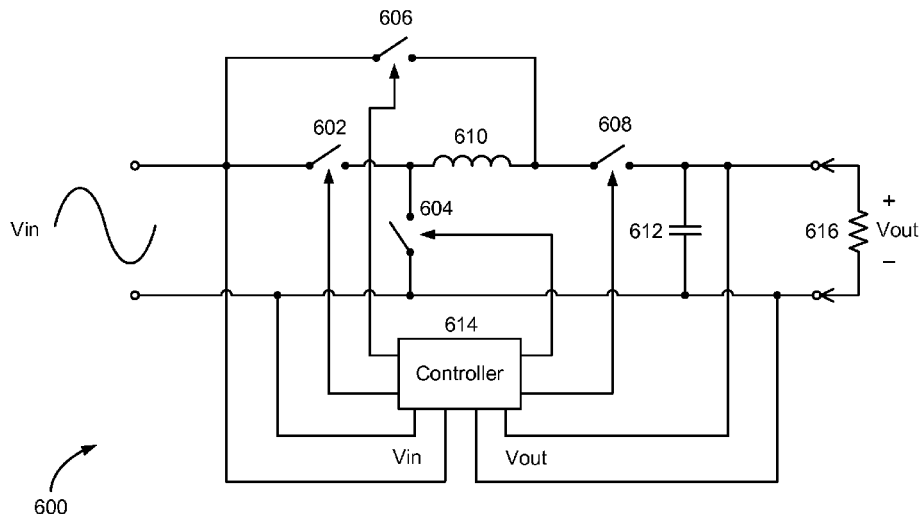
Assistant Examiner — Henry Lee, III

(74) *Attorney, Agent, or Firm* — William E. Winters; Patent Law Professionals, P.C.

(57) **ABSTRACT**

An AC/DC converter that converts an AC input voltage V_{in} to a DC output voltage comprises an inductor, a capacitor selectively coupled to the inductor, a plurality of switches, and a controller. The controller configures the plurality of switches, inductor, and capacitor to operate as a buck converter during times when $V_{in} > V_{out}$ and to operate as an inverting buck converter during times when $V_{in} < -V_{out}$. The controller modulates the duty cycles of the plurality of switches to regulate the DC output voltage V_{out} to the desired, constant output level.

24 Claims, 10 Drawing Sheets



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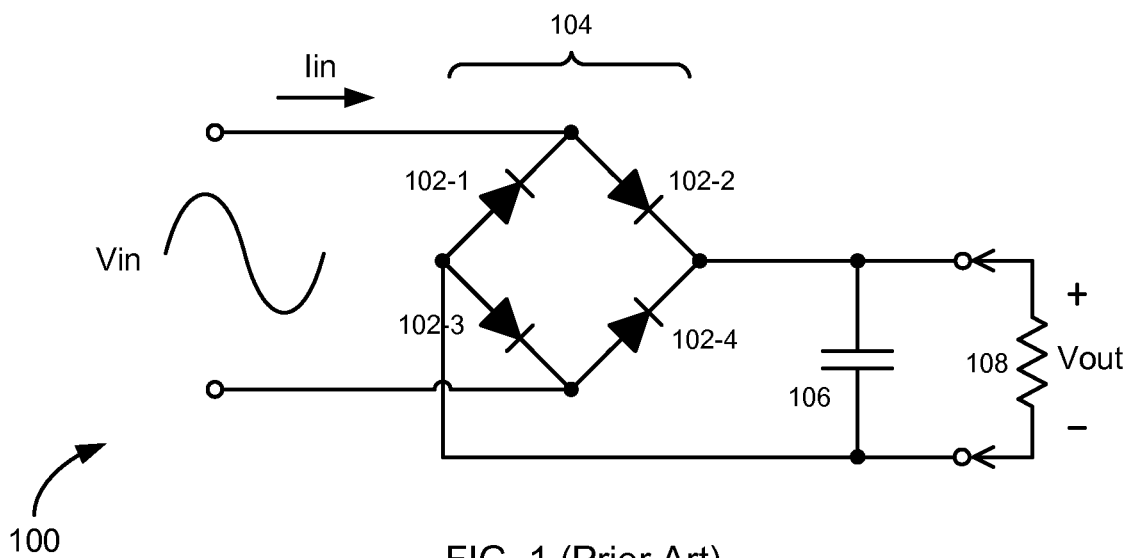
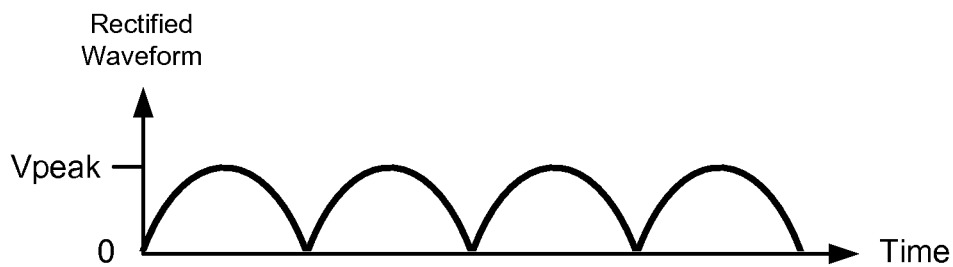
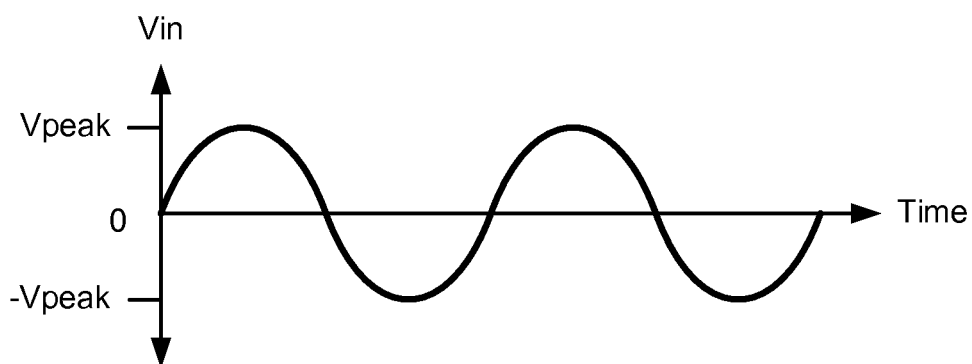


FIG. 1 (Prior Art)



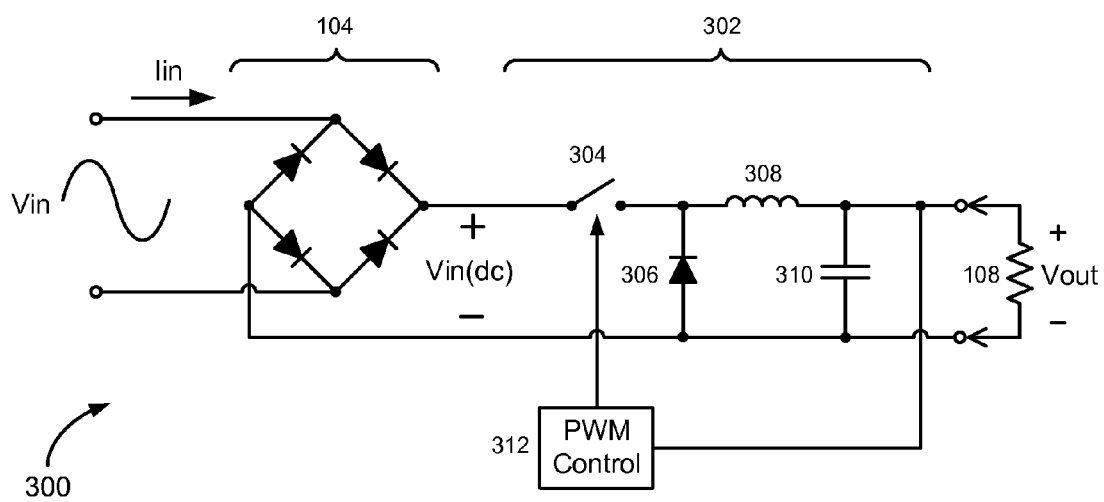


FIG. 3 (Prior Art)

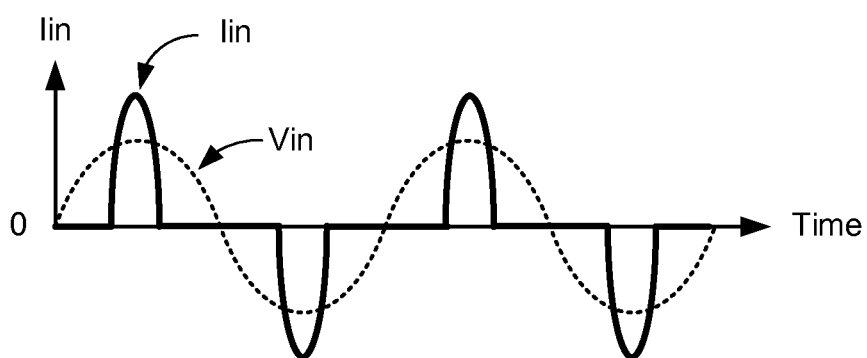


FIG. 4 (Prior Art)

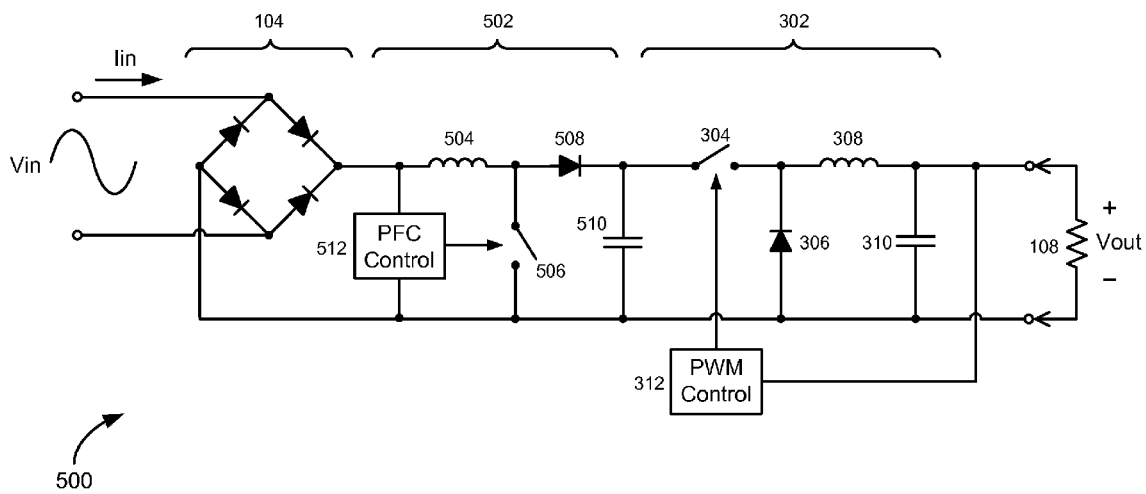


FIG. 5 (Prior Art)

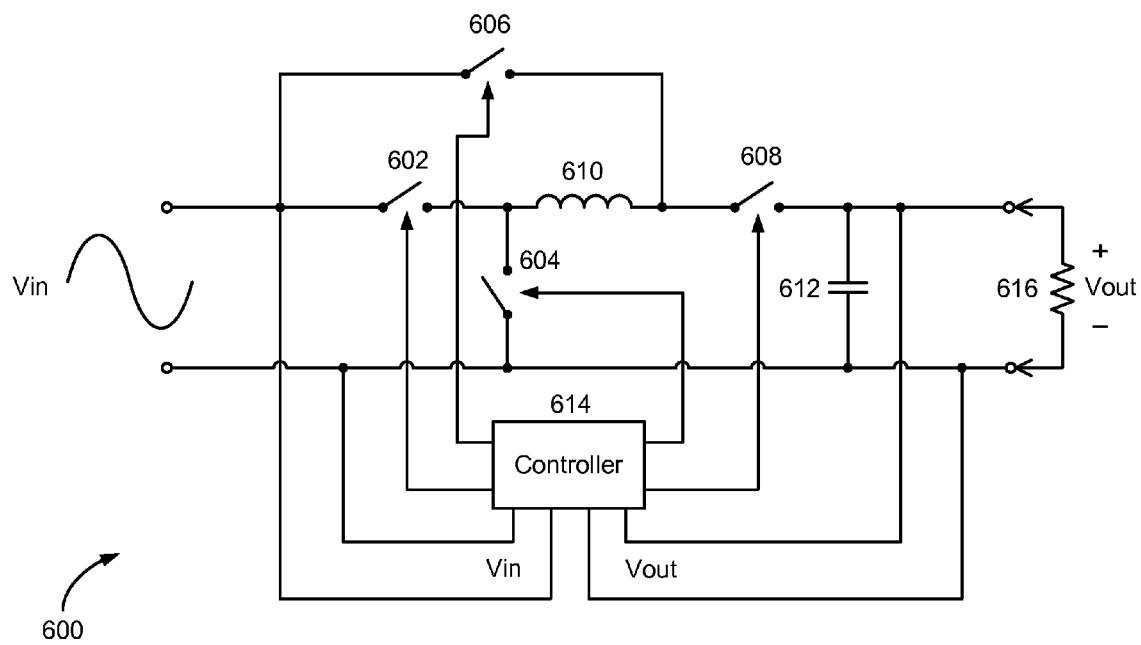


FIG. 6

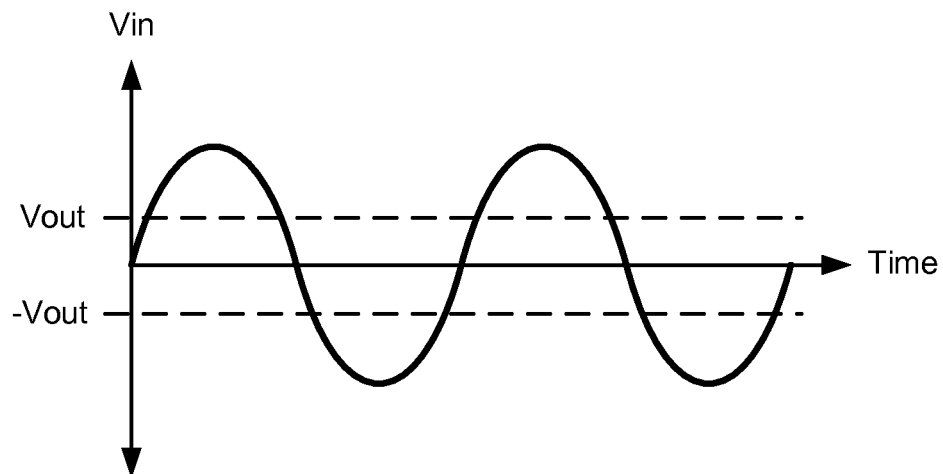


FIG. 7

Switch	$V_{in} > V_{out}$	$V_{in} < -V_{out}$	$ V_{in} < V_{out}$
602	D	OFF	OFF
604	1-D	ON	OFF
606	OFF	D	OFF
608	ON	1-D	OFF

FIG. 8

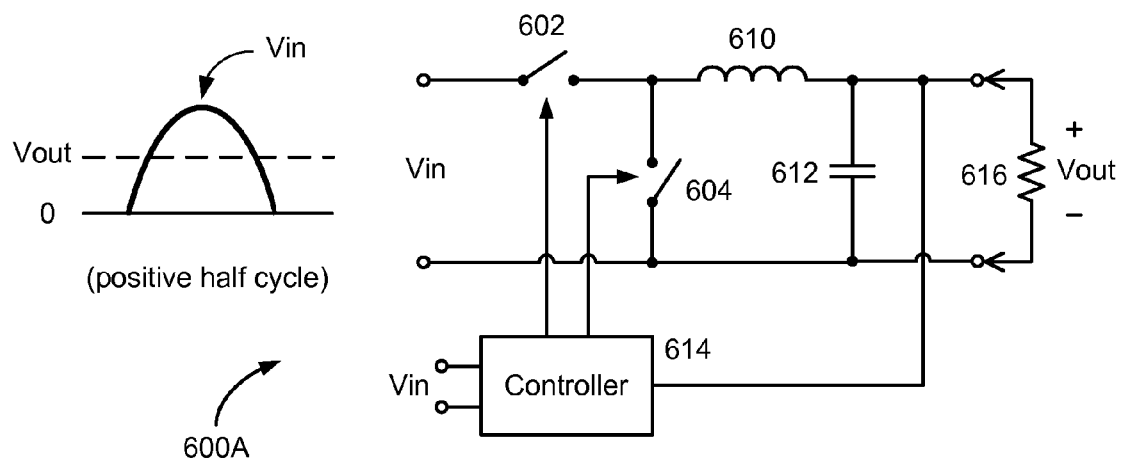


FIG. 9

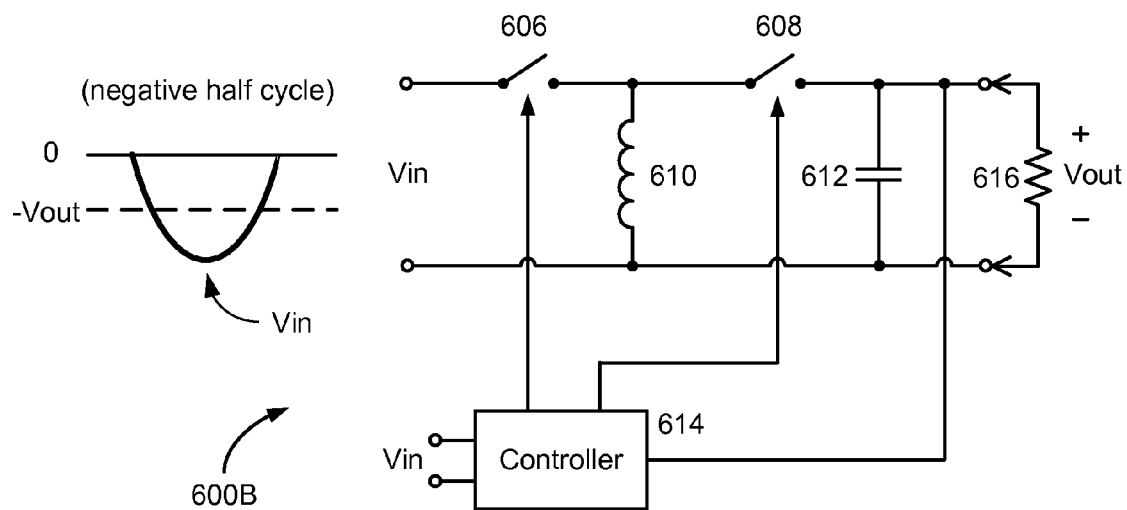


FIG. 10

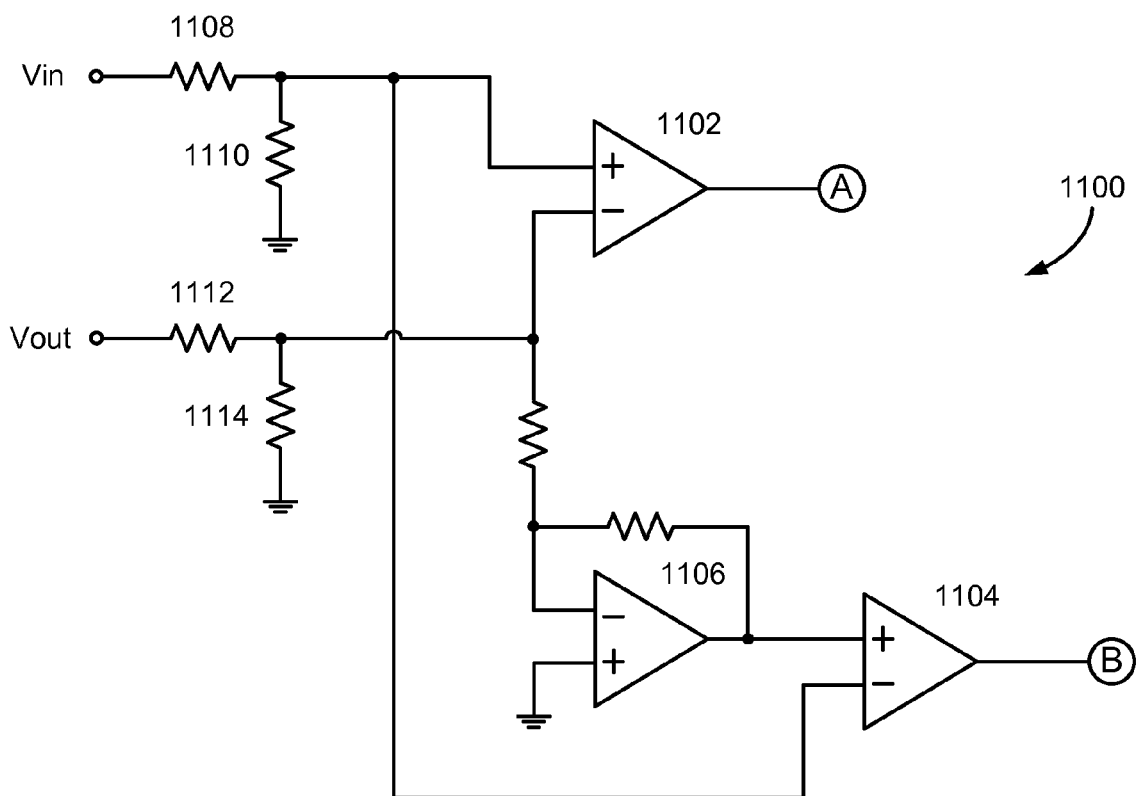


FIG. 11

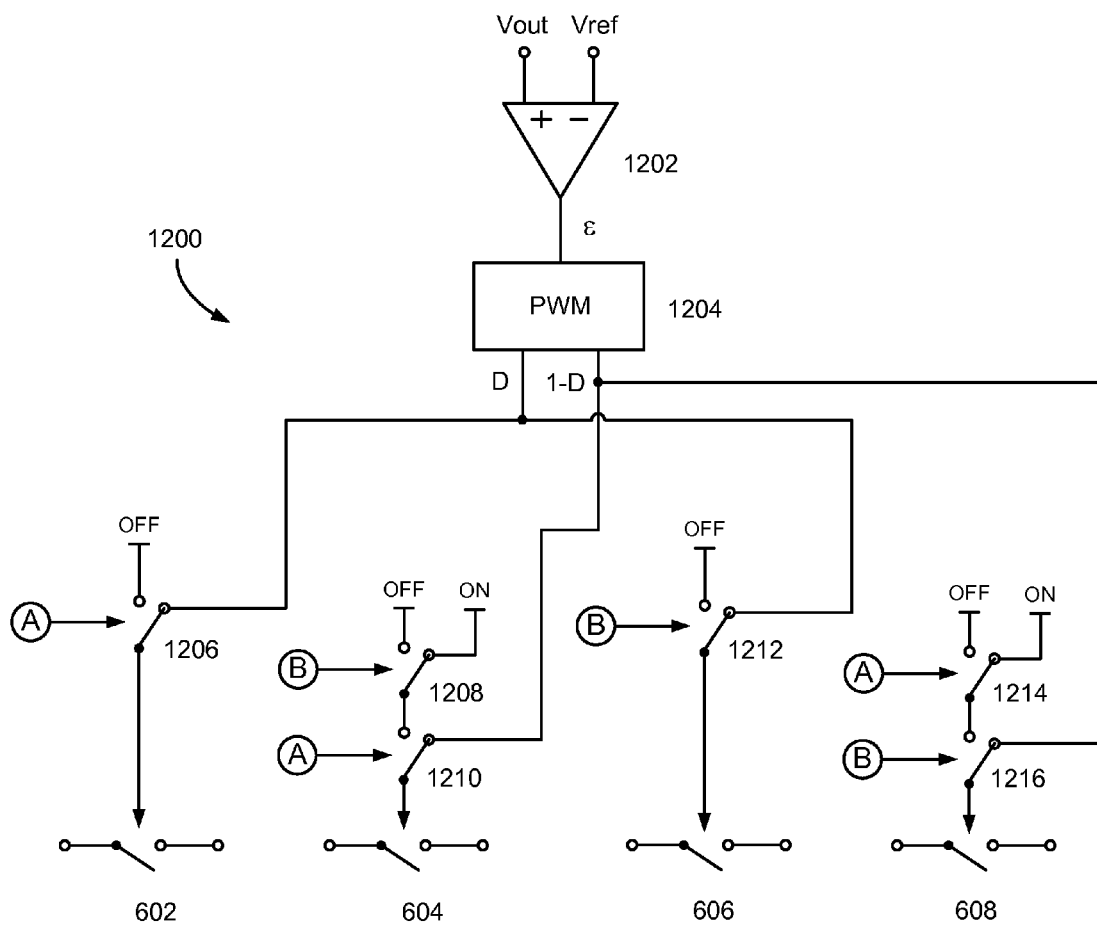


FIG. 12

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AC/DC POWER CONVERSION METHODS AND APPARATUS

FIELD OF THE INVENTION

The present invention relates in general to power conversion and in particular to methods and apparatus for converting alternating current (AC) to direct current (DC).

BACKGROUND OF THE INVENTION

Many household and industrial machines and devices are powered by a direct current (DC) power source that has been rectified from alternating current (AC) power provided by the AC mains. The AC-to-DC rectification is typically accomplished using a bridge rectifier **104** (or “diode bridge”) comprised of four diodes **102-1**, **102-2**, **102-3** **102-4** configured as shown in FIG. **1**. The bridge rectifier **104** converts the positive and negative half cycles of the AC input voltage V_{in} to a full-wave-rectified waveform of constant polarity. (See FIGS. **2A** and **2B**). To produce the desired steady DC output voltage V_{out} across a load **108**, the rectified waveform is filtered by a smoothing circuit, which in its simplest form comprises a smoothing capacitor **106** coupled to the output of the bridge rectifier **104**. The smoothing capacitor **106** functions to maintain the DC output voltage V_{out} near the peak voltage V_{peak} during the low portions of the AC input voltage V_{in} , as shown in FIG. **2C**. Some amount of AC ripple is superimposed on the DC output V_{out} , even following filtering by the smoothing capacitor **106**. The ripple may or may not be tolerable, depending on the application. In applications where it is not tolerable, additional filtering can be employed to reduce it to an acceptable level.

The AC/DC converter **100** in FIG. **1** generates a DC output voltage V_{out} near the peak voltage V_{peak} of the AC input voltage V_{in} (see FIG. **2C**). However, many applications require a much lower voltage. For example, many machines and devices require a DC voltage of 12 volts DC or less but the peak voltage V_{peak} of the center-tapped 120 volts RMS (root mean square) residential mains is near 170 V. To lower the DC voltage to the required level, a step-down transformer or DC-DC converter **302** (i.e., “buck converter”) is used. FIG. **3** illustrates use of a DC-DC converter **302**. The DC-DC converter **302** comprises a switch (typically a metal-oxide-semiconductor field effect transistor (MOSFET)) **304**, a diode (or, alternatively, a second MOSFET) **306**, an inductor **308**, a filter capacitor **310**, and a pulse-width modulator (PWM) control **312**. The PWM control **312** controls the opening and closing of the switch **304** at a fixed frequency f that is much higher than the 60 Hz line frequency (typically greater than 1 kHz). When the switch **304** is turned on, current flows through it, the inductor **308**, and then into the filter capacitor **310** and the load **108**. The increasing current causes the magnetic field of the inductor **308** to build up and energy to be stored in the inductor’s magnetic field. When the switch **304** is turned off, the voltage drop across the inductor **308** quickly reverses polarity and the energy stored by the inductor **308** is used as a current source for the load **108**. The DC output voltage V_{out} is determined by the proportion of time the switch **304** is on (t_{ON}) in each period T , where $T=1/f$. More specifically, $V_{out}=DV_{in}(dc)$, where $D=t_{ON}/T$ is known as the “duty cycle” and $V_{in}(dc)$ is the source DC input voltage provided at the output of the bridge rectifier **104**. The PWM control **312** is configured in a feed back path, allowing it to regulate the DC output voltage V_{out} by modulating the duty cycle D .

Although the AC/DC converter **300** in FIG. **3** addresses the inability of the AC/DC converter **100** in FIG. **1** to step down

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the DC voltage to a lower DC voltage, it does not address another well-known problem of conventional AC/DC converters—low power factor. The power factor of an AC/DC converter is a dimensionless number between 0 and 1 indicating how effectively real power from an AC power source is transferred to a load. An AC/DC converter with a low power factor draws more current from the mains than one having a high power factor for the same amount of useful power transferred. A low power factor can result due to the input voltage V_{in} being out of phase with the input current I_{in} or by action of a nonlinear load distorting the shape of the input current I_{in} . The latter situation arises in non-power-factor-corrected AC/DC converters, such as those described in FIGS. **1** and **3**, which as described above use a diode bridge **104**. The filter capacitor **106** of the AC/DC converter **100** in FIG. **1** (and, similarly, the filter capacitor **310** of the AC/DC converter **300** in FIG. **3**) remains charged near the peak voltage V_{peak} for most of the time. This means that the instantaneous AC line voltage V_{in} is below the filter capacitor **106** voltage for most of the time. The diodes **102-1**, **102-2**, **102-3** **102-4** of the bridge rectifier **104** therefore conduct only for a small portion of each AC half-cycle, resulting in the input current I_{in} drawn from the mains being a series of narrow pulses, as illustrated in FIG. **4**. Note that although the input current I_{in} is in phase with the AC input voltage V_{in} , it is distorted and, therefore, rich in harmonics of the line frequency. The harmonics lower the power factor, resulting in reduced conversion efficiency and undesirable heating in the AC mains generator and distribution systems. The harmonics also create noise that can interfere with the performance of other electronic equipment.

To reduce harmonics and increase the power factor, conventional AC/DC converters are often equipped with a power factor correction (PFC) pre-regulator. The PFC pre-regulator can be formed in various ways. One approach employs a PFC boost converter **502** coupled between the bridge rectifier **104** and the DC-DC converter **302**, as shown in the power-factor-corrected AC/DC converter **500** in FIG. **5**. The PFC boost converter **502** comprises an inductor **504**, switch **506**, diode **508**, output capacitor **510** and a PFC control **512**. The PFC control **512** controls the on and off state of the switch **506**. When the switch **506** is switched on, current from the mains flows through the inductor **504**, causing energy to build up and be stored in the inductor’s magnetic field. During this time, current to the DC-DC converter **302** and load **108** is supplied by the charge in the capacitor **510**. When the switch **506** is turned off, the voltage across the inductor **504** quickly reverses polarity to oppose any drop in current, and current flows through the inductor **504**, the diode **508** and to the DC-DC converter **302**, recharging the capacitor **510** as well. With the polarity reversed, the voltage across the inductor **504** adds to the source input DC voltage, thereby boosting the input DC voltage. The PFC boost converter **502** output voltage is dependent on the duty cycle D of the on-off switch control signal provided by the PFC control circuit **512**. More specifically, the PFC boost converter **502** output voltage is proportional to $1/(1-D)$, where D is the duty cycle and $(1-D)$ is the proportion of the switching cycle T (i.e., commutation period) that switch **506** is off. In addition to setting the duty cycle D , the PFC control **512** forces the DC-DC converter **302** and load **108** to draw current that on average follows the sinusoidal shape of the AC input voltage V_{in} , thereby reducing harmonics and increasing the power factor of the AC/DC converter **500**.

The power-factor-corrected AC/DC converter **500** is suitable for many applications. However, it has a number of drawbacks. First, the AC/DC converter is less efficient than desired, particularly since the AC-to-DC power conversion

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requires two stages—the PFC boost converter **502** front end and the DC-DC converter **302** final stage. Second, the converter **500** has a large parts count, including parts necessary to implement the two control circuits (PFC control **512** and PWM control **312**), which increases design complexity and cost, and makes the converter **500** more susceptible to failure. Third, the PFC boost converter **502** generates very high voltages, which stress the converter's parts and raise safety concerns.

It would be desirable, therefore, to have AC/DC conversion methods and apparatus that are efficient at converting AC to DC, avoid power factor degradation attributable to using a bridge rectifier, do not require voltage boosters to counteract power factor degradation, and do not have a large parts count.

SUMMARY OF THE INVENTION

Methods and apparatus for converting alternating current (AC) to direct current (DC) are disclosed. An exemplary AC/DC converter that converts an AC input voltage V_{in} , such as may be provided by the AC mains, to a DC output voltage comprises an inductor, a capacitor, a plurality of switches, and a controller. The controller configures the plurality of switches, inductor, and capacitor to operate as a buck converter during times when $V_{in} > V_{out}$ and to operate as an inverting buck converter during times when $V_{in} < -V_{out}$. The controller modulates the duty cycles of the plurality of switches to regulate the DC output voltage V_{out} to the desired, constant output level.

The AC/DC converter of the present invention converts the AC input voltage V_{in} to the DC output voltage V_{out} directly, i.e., without the need for a bridge rectifier or transformer to complete the AC-to-DC conversion. Direct AC to DC conversion avoids power factor degradation problems attributable to use of bridge rectifiers, obviates the need for specialized power factor correction pre-regulator circuitry, and results in a low parts count and an energy-efficient design.

Further features and advantages of the invention, including descriptions of the structure and operation of the above-summarized and other exemplary embodiments of the invention, will now be described in detail with respect to accompanying drawings, in which like reference numbers are used to indicate identical or functionally similar elements.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a circuit diagram of a conventional alternating current to direct current (AC/DC) converter;

FIG. 2A is a signal diagram of the AC input voltage V_{in} applied to the AC input of the AC/DC converter in FIG. 1;

FIG. 2B is a signal diagram of the unfiltered, full-wave-rectified voltage waveform produced at the output of the bridge rectifier of the AC/DC converter in FIG. 1;

FIG. 2C is a signal diagram of the DC output voltage of the AC/DC converter in FIG. 1 after having been filtered by a smoothing capacitor;

FIG. 3 is a circuit diagram of an AC/DC converter equipped with a step-down buck converter to step down the DC output voltage to a level lower than possible using just a bridge rectifier and smoothing capacitor;

FIG. 4 is a signal diagram illustrating how the bridge rectifier used by the AC/DC converters in FIGS. 1 and 3 causes current to be drawn from the AC power source in narrow pulses that are rich in harmonics;

FIG. 5 is a circuit diagram of an AC/DC converter having a step-down buck converter and a power-factor-correcting

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boost converter that compensates for power factor degradation caused by the AC/DC converter's bridge rectifier;

FIG. 6 is a circuit diagram of an AC/DC converter, according to an embodiment of the present invention;

FIG. 7 is a signal diagram of the AC input voltage V_{in} supplied to the AC/DC converter in FIG. 6 and its relationship to the DC output voltage V_{out} generated by the AC/DC converter and its inverse $-V_{out}$;

FIG. 8 is a table showing how the switches of the AC/DC converter in FIG. 6 are switched and driven, depending on the instantaneous value of the AC input voltage V_{in} compared to the DC output voltage V_{out} generated by the AC/DC converter in FIG. 6 and its inverse $-V_{out}$;

FIG. 9 is a circuit diagram illustrating how the AC/DC converter in FIG. 6 reduces to and operates as a buck converter during times of positive half cycles of the AC input voltage when $V_{in} > V_{out}$;

FIG. 10 is a circuit diagram illustrating how the AC/DC converter in FIG. 6 reduces to and operates as an inverting buck converter during times of negative half cycles of the AC input voltage when $V_{in} < -V_{out}$;

FIG. 11 is a circuit diagram of a comparison circuit that forms part of the controller of the AC/DC converter in FIG. 6 and which compare the AC input voltage V_{in} to the DC output voltage V_{out} to determine times whether $V_{in} > V_{out}$ and $V_{in} < -V_{out}$; and

FIG. 12 is a circuit diagram of a switch control circuit that forms part of the controller of the AC/DC converter in FIG. 6 and which operates to control the switching of the switches of the AC/DC converter in FIG. 6.

DETAILED DESCRIPTION

Referring to FIG. 6, there is shown an alternating current to direct current (AC/DC) converter **600**, according to an embodiment of the present invention. The AC/DC converter **600** comprises first, second, third and fourth switches **602**, **604**, **606** and **608**, an inductor **610**, a smoothing capacitor **612**, and a controller **614**. The first switch **602** is coupled between one terminal of the AC input and a first terminal of the inductor **610**; the second switch **604** is coupled between the first terminal of the inductor **610** and the opposing-polarity terminal of the AC input; the third switch **606** is coupled between the AC input and the second terminal of the inductor **610**; and the fourth switch **608** is coupled between the second terminal of the inductor **610** and the positive DC output terminal. The controller **614** generates switch drive signals for controlling the switching of the first, second, third and fourth switches **602**, **604**, **606** and **608**, depending on the instantaneous AC input voltage V_{in} compared to the DC output voltage, and selectively modulates the duty cycles of the first, second, third and fourth switches **602**, **604**, **606** and **608** so that the DC output voltage V_{out} is maintained at the desired level, as is explained in more detail below.

The components of the AC/DC converter **600** comprise discrete devices, one or more integrated circuit (IC) chips, or a combination of discrete devices and IC chips. In one embodiment, the controller **614** and first, second, third, and fourth switches **602**, **604**, **606** and **608** are integrated in a single IC chip manufactured in accordance with a standard complementary metal-oxide-semiconductor (CMOS) fabrication process, with the first, second, third, and fourth switches **602**, **604**, **606** and **608** comprising metal-oxide-semiconductor field-effect transistors (MOSFETs). In another embodiment, the first, second, third, and fourth switches **602**, **604**, **606** and **608** are formed in a first IC chip and the controller is formed in a second IC chip. Whereas the

first, second, third, and fourth switches **602**, **604**, **606** and **608** comprise silicon-based MOSFETs in the exemplary embodiment just described, other types of switching devices may be used, including conventional switches, diodes, relays, or other semiconductor-based or non-semiconductor-based switching devices. For example, in applications requiring fast switching speeds, compound-semiconductor-based transistor devices, such as high electron mobility transistors (HEMTs) or heterojunction bipolar transistors (HBTs), may be used to implement the first, second, third, and fourth switches **602**, **604**, **606** and **608** switches, instead of silicon-based MOSFETs. For the purpose of this disclosure, the term “switch” is used in its broadest sense to include all of these types of switches and any other suitable switching device. The inductor **610** and capacitor **612** may also be integrated in the one or more IC chips, or either or both of these devices may be discrete devices coupled to external pins of the one or more IC chips.

The AC/DC converter **600** is configured to directly convert an AC input voltage V_{in} , such as may be provided by the AC mains, to a DC output voltage V_{out} , without the need for a diode bridge or a step-down transformer. Direct conversion is accomplished by controlling and modulating the on/off states of the first, second, third, and fourth switches **602**, **604**, **606** and **608** using the controller **614**. More specifically, depending on the instantaneous AC input voltage V_{in} compared to the DC output voltage V_{out} , the switches are turned on (closed), turned off (opened), driven by a switch drive signal of duty cycle D , or driven by a complementary switch drive signal of duty cycle $(1-D)$. The switch drive signal (labeled “ D ” in FIG. 6) and the complementary switch drive signal (labeled “ $1-D$ ” in FIG. 6) are periodic (or semi-periodic) and have a common, fixed switching frequency $f=1/T$, where T is the switching period. As illustrated in the signal diagram in FIG. 7 and shown in the switching table in FIG. 8, when $V_{in}>V_{out}$, the first switch **602** is driven by the switch drive signal at a duty cycle $t_{ON}/T=D$, the second switch **604** is driven by the complementary switch drive signal at a duty cycle $(T-t_{ON})/T=(1-D)$, the third switch **606** is turned off, and the fourth switch **608** is turned on. When $V_{in}<-V_{out}$, the first switch **602** is turned off, the second switch **604** is turned on, the third switch **606** is driven by the switch drive signal at a duty cycle D , and the fourth switch is driven by the complementary switch drive signal at a duty cycle $(1-D)$. Finally, when V_{in} is greater than $-V_{out}$ but less than V_{out} , i.e. when $|V_{in}|<V_{out}$, the first, second, third, and fourth switches **602**, **604**, **606** and **608** are turned off.

The DC output voltage of the AC/DC converter **600** is equal to $D|V_{in}|$, where $|V_{in}|$ is the absolute value of the instantaneous AC input voltage. According to one embodiment, the controller **614** modulates the duty cycle D , regulating the DC output voltage V_{out} so that it is maintained at a constant level. The duty cycle D may also be managed to improve the power factor of the AC/DC converter **600**. Whereas D is modulated to maintain the DC output voltage V_{out} at a constant level in the exemplary embodiment described here, in general V_{out} , D , and V_{in} are all variables. Accordingly, V_{out} need not necessarily be maintained at a constant level.

That $V_{out}=D|V_{in}|$ is more readily apparent by understanding that the AC/DC converter **600** comprises an integrated (i.e., conjoined) buck converter and an inverting buck converter. During the positive half cycles of the AC input waveform when $V_{in}>V_{out}$, the third switch **606** is off, the fourth switch **608** is on, and the AC/DC converter **600** reduces to and operates as a buck converter **600A**, as illustrated in FIG. 9. The first and second switches **602** and **604** serve as the high-side and low-side switches of the buck converter and are

driven by the switch drive signal at duty cycle D and complementary switch drive signal at a duty cycle $(1-D)$, respectively. The first and second switches **602** and **604** therefore alternately configure the inductor **610** between storing energy and supplying current during positive half cycles of the AC input voltage when $V_{in}>V_{out}$, and the DC output voltage $V_{out}=DV_{in}$.

During the negative half cycles of the AC input waveform when $V_{in}<-V_{out}$, the first switch **602** is off, the second switch **604** is on, and the AC/DC converter **600** reduces to and operates as what may be referred to as an “inverting” buck converter **600B**, as illustrated in FIG. 10. The third and fourth switches **606** and **608** are driven by the switch drive signal D and complementary switch drive signal $(1-D)$, respectively. The inverting buck converter **600B** inverts the negative input voltage V_{in} , alternately configuring, by the switching action of the third and fourth switches **606** and **608**, the inductor **610** between storing energy and supplying current during the negative half cycles of the AC input voltage when $V_{in}<-V_{out}$, to produce an output voltage V_{out} equal to $D|V_{in}|$. Hence, considering both positive and negative half cycles, the AC/DC converter **600** produces a DC output voltage $V_{out}=D|V_{in}|$.

The controller **614** of the AC/DC converter **600** includes a comparison circuit that continually compares the AC input voltage V_{in} to the DC output voltage V_{out} , to determine whether $V_{in}>V_{out}$ or $V_{in}<-V_{out}$. FIG. 11 is a drawing of an exemplary comparison circuit **1100** that performs this task. The comparison circuit **1100** comprises first and second comparators **1102** and **1104**, an inverting amplifier **1106**, a first voltage divider including resistors **1108** and **1110**, and a second voltage divider including resistors **1112** and **1114**. The first voltage divider scales the AC input voltage down to a scaled AC input voltage αV_{in} so that the voltage is within the acceptable input voltage range limit of the first comparator **1102**. The second voltage divider scales the DC output voltage down by the same amount to produce a scaled DC output voltage αV_{out} . The first comparator **1102** compares the scaled AC input voltage αV_{in} to the scaled DC output voltage αV_{out} , producing a high output voltage when $V_{in}>V_{out}$ and a low output voltage when $V_{in}<V_{out}$. The inverting amplifier **1106** inverts the scaled DC output voltage αV_{out} to produce a scaled and inverted DC output voltage $-\alpha V_{out}$. The second comparator **1104** compares the scaled and inverted DC output voltage $-\alpha V_{out}$ to the scaled AC input voltage αV_{in} , producing a high output voltage when $V_{in}<-V_{out}$ and a low output voltage when $V_{in}>-V_{out}$.

The controller **614** of the AC/DC converter **600** also includes a switch control circuit **1200**, shown in FIG. 12, which controls the switching of the first, second, third, and fourth switches **602**, **604**, **606** and **608**. The switch control circuit **1200** comprises an error amplifier **1202**, a pulse-width modulator (PWM) **1204**, and switches **1206-1216** having on/off states that control the switching of the first, second, third and fourth switches **602**, **604**, **606** and **608**. The error amplifier **1202** compares the DC output voltage V_{out} to a precise reference voltage V_{ref} that is equal to and defines the desired DC output voltage V_{out} and produces an error signal ϵ based on the difference between V_{ref} and V_{out} . The PWM **1204** generates the aforementioned switch drive signal (labeled “ D ” in FIG. 12) and complementary switch drive signal (labeled “ $1-D$ ” in FIG. 12) and modulates D based on the error signal ϵ , thereby providing the switch control circuit **1200** the ability to regulate the DC output voltage V_{out} . The switches **1206-1216** are controlled by the outputs of the first and second comparators **1102** and **1104** of the comparator circuit **1100** in FIG. 11 and control the switching states of the first,

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second, third and fourth switches **602**, **604**, **606** and **608**, in accordance with the switching table in FIG. **8**.

In the exemplary embodiment above, the switch control circuit **1200** is described as controlling the opening and closing of the switches **606**, **604**, **606** and **608**, according to the switching table in FIG. **8**. In another embodiment, the controller **614** is alternatively or further configured to hold switch **608** open during light load conditions. (What defines the light load condition is dependent on the application and established and set during design.) The remaining switches **602**, **604** and **606** are configured to operate according to the switching table in FIG. **8**, or are configured to not switch at all, with no effect on the load **616**. Hence, during light load conditions, the capacitor **612** serves as the power supply for the load **616**.

While various embodiments of the present invention have been described, they have been presented by way of example and not limitation. It will be apparent to persons skilled in the relevant art that various changes in form and detail may be made to the exemplary embodiments without departing from the true spirit and scope of the invention. Accordingly, the scope of the invention should not be limited by the specifics of the exemplary embodiments. Rather, the scope of the invention should be determined by the appended claims, including the full scope of equivalents to which such claims are entitled.

What is claimed is:

1. An AC/DC converter for converting an AC input voltage V_{in} to a DC output voltage V_{out} , comprising:

an inductor;

first and second switches that, only during positive half cycles of the AC input voltage when $V_{in} > V_{out}$, alternately configure said inductor between storing energy and supplying current;

third and fourth switches that, only during negative half cycles of the AC input voltage when $V_{in} < -V_{out}$, alternately configure said inductor between storing energy and supplying current; and

a controller configured to control said first, second, third and fourth switches.

2. The AC/DC converter of claim **1** wherein said controller includes a comparison circuit configured to compare the AC input voltage V_{in} to the DC output voltage V_{out} .

3. The AC/DC converter of claim **2** wherein said controller further includes a switch control circuit that controls the switching of said first, second, third and fourth switches depending on comparisons of the AC input voltage V_{in} to the DC output voltage V_{out} .

4. The AC/DC converter of claim **1** where said controller includes a switch control circuit that controls the switching of said first, second, third and fourth switches depending on the AC input voltage V_{in} compared to the DC output voltage V_{out} .

5. The AC/DC converter of claim **1** wherein only during positive half cycles of the AC input voltage when $V_{in} > V_{out}$ said controller is configured to switch said first switch on and off at frequency f and duty cycle D , and is configured to switch said second switch on and off at the frequency f and duty cycle $(1-D)$.

6. The AC/DC converter of claim **5** wherein only during negative half cycles of the AC input voltage when $V_{in} < -V_{out}$ said controller is configured to switch said third switch on and off at the frequency f and duty cycle D , and is configured to switch said fourth switch on and off at the frequency f and duty cycle $(1-D)$.

7. The AC/DC converter of claim **6** wherein said controller includes a pulse-width modulator configured to modulate D and regulate the DC output voltage V_{out} .

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8. An AC/DC converter for converting an AC input voltage V_{in} to a DC output voltage V_{out} , comprising:

an inductor;

a capacitor selectively coupled to said inductor;

a plurality of switches; and

a controller that configures the plurality of switches, inductor and capacitor to operate as a buck converter during times when $V_{in} > V_{out}$, and configures the plurality of switches, inductor and capacitor to operate as an inverting buck converter during times when $V_{in} < -V_{out}$, wherein said inductor is the only inductor needed by said AC/DC converter to convert said AC input voltage V_{in} to said DC output voltage V_{out} .

9. The AC/DC converter of claim **8** wherein said plurality of switches includes first and second switches that serve as buck switches of the buck converter but only during the times when $V_{in} > V_{out}$.

10. The AC/DC converter of claim **9** wherein said plurality of switches further includes third and fourth switches that serve as inverting buck switches of the inverting buck converter but only during the times when $V_{in} < -V_{out}$.

11. The AC/DC converter of claim **8** wherein said plurality of switches includes first, second, third and fourth switches and said controller is configured to:

switch said first and second switches on and off at a common frequency f and at a duty cycle D and duty cycle $(1-D)$, respectively, but only during the times when $V_{in} > V_{out}$; and

switch said third and fourth switches on and off at the common frequency f and at the duty cycle D and duty cycle $(1-D)$, respectively, but only during the times when $V_{in} < -V_{out}$.

12. The AC/DC converter of claim **11** wherein said controller includes a pulse-width modulator configured to regulate the DC output voltage by modulating the duty cycle D of the first and third switches and by modulating the duty cycle $(1-D)$ of the second and fourth switches.

13. A method of converting an AC input voltage V_{in} to a DC output voltage V_{out} , comprising:

converting the AC input voltage during positive half cycles to the DC output voltage V_{out} using a buck converter; and

converting the AC input voltage during negative half cycles to the DC output voltage V_{out} using an inverting buck converter,

wherein said buck converter and said inverting buck converter share an inductor and said shared inductor is the only inductor needed by said buck converter and said inverting buck converter to convert said AC input voltage V_{in} to said DC output voltage V_{out} .

14. The method of claim **13** wherein converting the AC input voltage to the DC output voltage during the positive and negative half cycles are performed by modulating duty cycles of switches of said buck converter and said inverting buck converter.

15. The method of claim **13** wherein converting positive half cycles of the AC input voltage to the DC output voltage V_{out} using the buck converter comprises:

determining times when $V_{in} > V_{out}$; and

for times it is determined that $V_{in} > V_{out}$, converting the AC input voltage to the DC output voltage V_{out} .

16. The method of claim **13** wherein converting negative half cycles of the AC input voltage to the DC output voltage V_{out} using an inverting buck converter comprises:

determining times when $V_{in} < -V_{out}$; and

for times it is determined that $V_{in} < -V_{out}$, converting the AC input voltage to the DC output voltage V_{out} .

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17. The method of claim 13 wherein the buck converter and inverting buck converter comprise a conjoined buck and inverting buck converter circuit that shares said inductor.

18. An AC/DC converter for converting an AC input voltage V_{in} to a DC output voltage V_{out} , comprising:

means for determining times when $V_{in} > V_{out}$ and times when $V_{in} < -V_{out}$;

first converting means for converting the AC input voltage during positive half cycles to the DC output voltage V_{out} during times when $V_{in} > V_{out}$; and

second converting means for converting the AC input voltage during negative half cycles to the DC output voltage V_{out} during times when $V_{in} < -V_{out}$.

19. The AC/DC converter of claim 18, further comprising means for controlling said first converting means and said second converting means.

20. The AC/DC converter of claim 19 wherein:

said first converting means includes first switching means; said second converting means includes second switching means; and

said means for controlling is configured to control said first and second switching means to maintain the DC output voltage V_{out} at a constant level.

21. An AC/DC converter for converting an AC input voltage V_{in} to a DC output voltage V_{out} , comprising:

an inductor;

a first plurality of switches configured to alternately couple and decouple said inductor to and from an AC input voltage during positive half cycles of the AC input voltage; and

a second plurality of switches configured to alternately couple and decouple said inductor to and from the AC input voltage during negative half cycles of the AC input voltage,

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wherein said inductor and said second plurality of switches are configured as an inverting buck converter during times when $V_{in} < -V_{out}$.

22. An AC/DC converter for converting an AC input voltage V_{in} to a DC output voltage V_{out} , comprising:

an inductor;

a first plurality of switches configured to alternately couple and decouple said inductor to and from an AC input voltage during positive half cycles of the AC input voltage; and

a second plurality of switches configured to alternately couple and decouple said inductor to and from the AC input voltage during negative half cycles of the AC input voltage,

wherein all switches of said first and second pluralities of switches are configured to remain off during times when $|V_{in}| < V_{out}$.

23. The AC/DC converter of claim 1 wherein said inductor is the only inductor needed to convert said AC input voltage V_{in} to said DC output voltage V_{out} .

24. An AC/DC converter for converting an AC input voltage V_{in} to a DC output voltage V_{out} , comprising:

an inductor;

a first plurality of switches configured to alternately couple and decouple said inductor to and from an AC input voltage during positive half cycles of the AC input voltage; and

a second plurality of switches configured to alternately couple and decouple said inductor to and from the AC input voltage during negative half cycles of the AC input voltage,

wherein said inductor is the only inductor needed to convert said AC input voltage V_{in} to said DC output voltage V_{out} .

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